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(54) Abstract Title

Drillpipe structures to accomodate downhole testing

(57) A drill collar structure 10 to facilitate measurement-while-drilling (MWD) techniques while at the same time having sufficient rigidity to facilitate the drilling operation is disclosed. In some embodiments, a metal structure involving openings such as slots, preferably oriented longitudinally along its axis, but also in other configurations, are disclosed to allow sufficient strength while at the same time allowing exit and entrance of electromagnetic energy. A composite structure is also disclosed which, for given layers, has adjacent fibers such as glass 12 and carbon 14, 16, so that when the layers are overlapped, glass areas overlap glass areas throughout the radial thickness of the composite tube to create "windows" for the entrance and exit of electromagnetic energy. In yet other embodiments, the drill collar 10 can be made of a metallic frame structure with a multiplicity of openings which are filled with a composite material. The metallic frame structure provides structural rigidity while the openings, filled with composite material which are attached to the metal structure, form a fluid-tight cohesive structure sufficient to withstand the rigors of drilling, while at the same time allow the measurements of the formation to be taken through the windows or by making use of sensors embedded in the windows. In another alternative composite structure, carbon fibers can be used if they are electrically insulated in the areas where electromagnetic energy is to enter and exit the structure. Another composite alternative is to alternate carbon and glass fibers in particular sequences or to use insulated carbon fibers to facilitate the operation of instruments which can be mounted in the structure whose operation could be negatively affected by conductivity in the wall in an azimuthal direction.

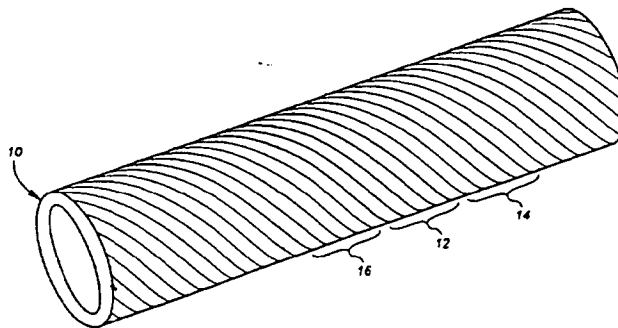


FIG. 1

At least one drawing originally filed was informal and the print reproduced here is taken from a later filed formal copy.

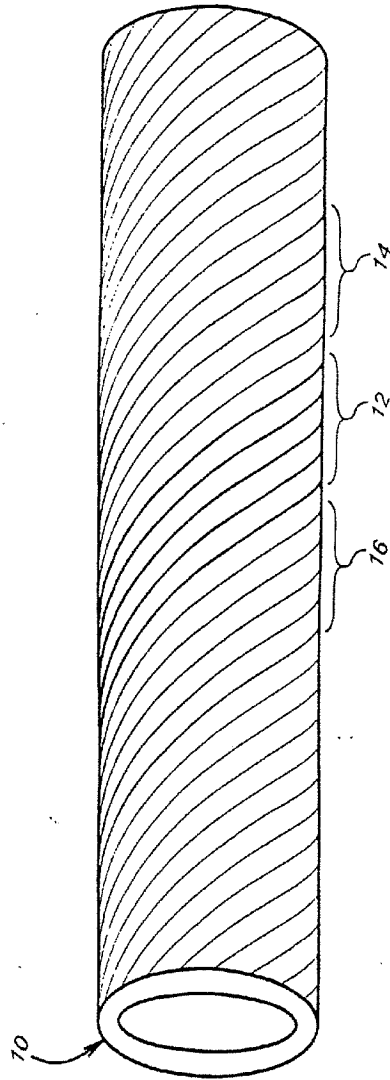
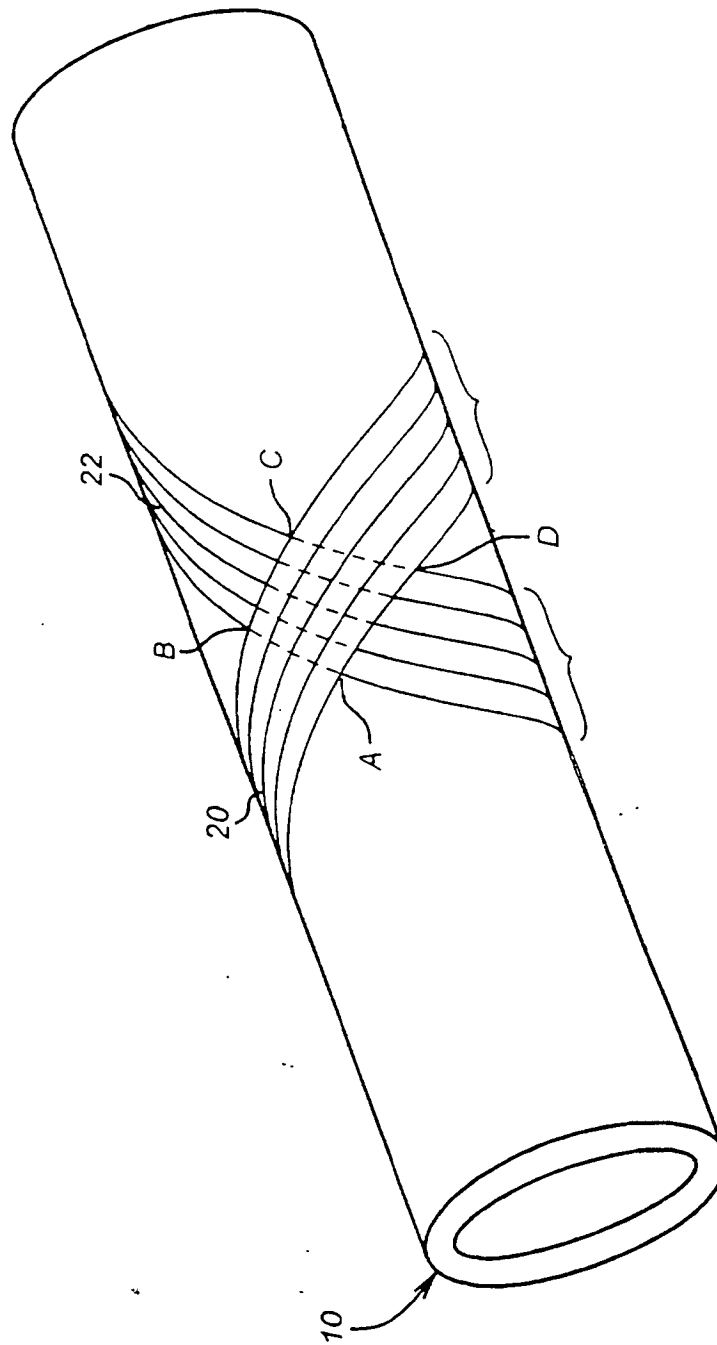


FIG. 1

**FIG. 2**

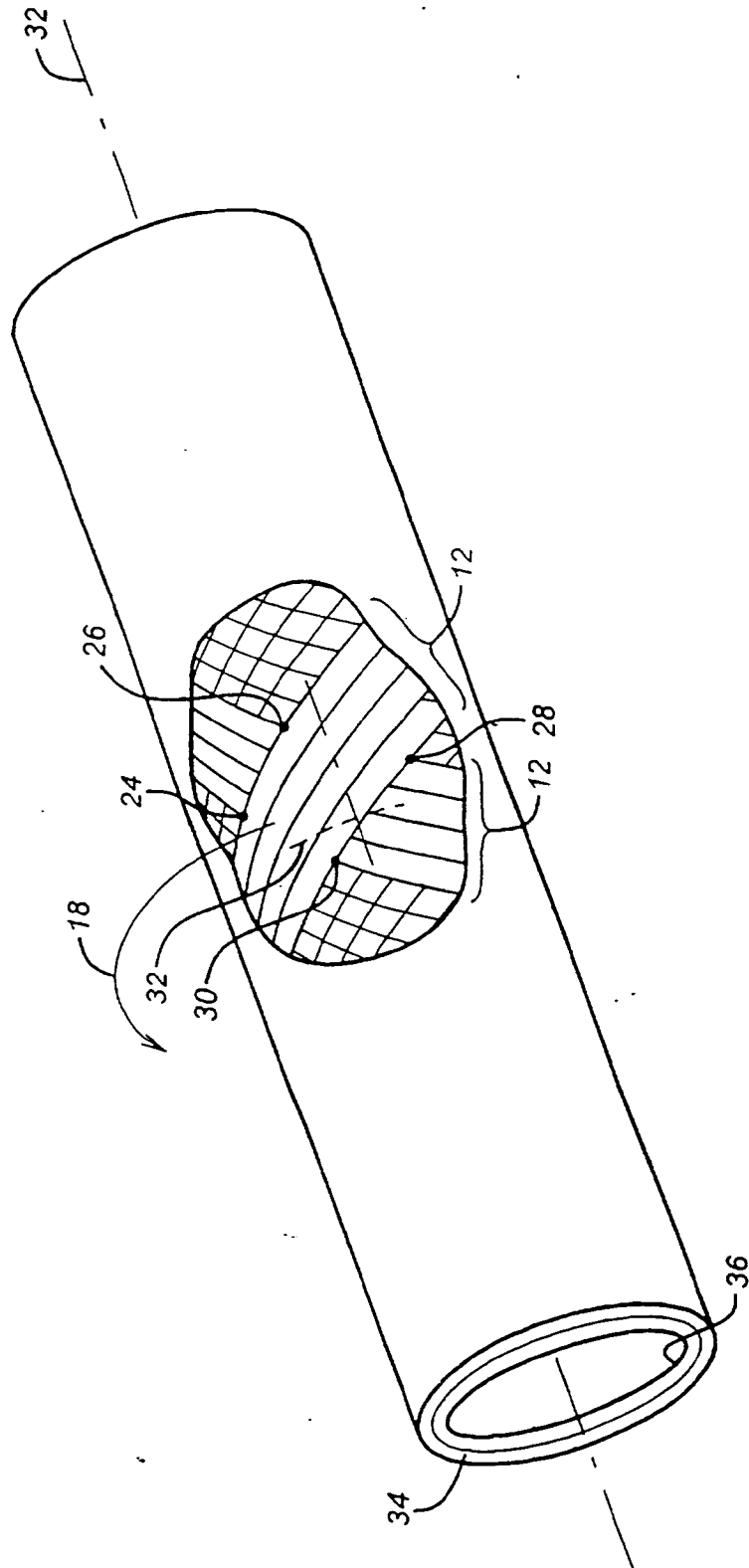
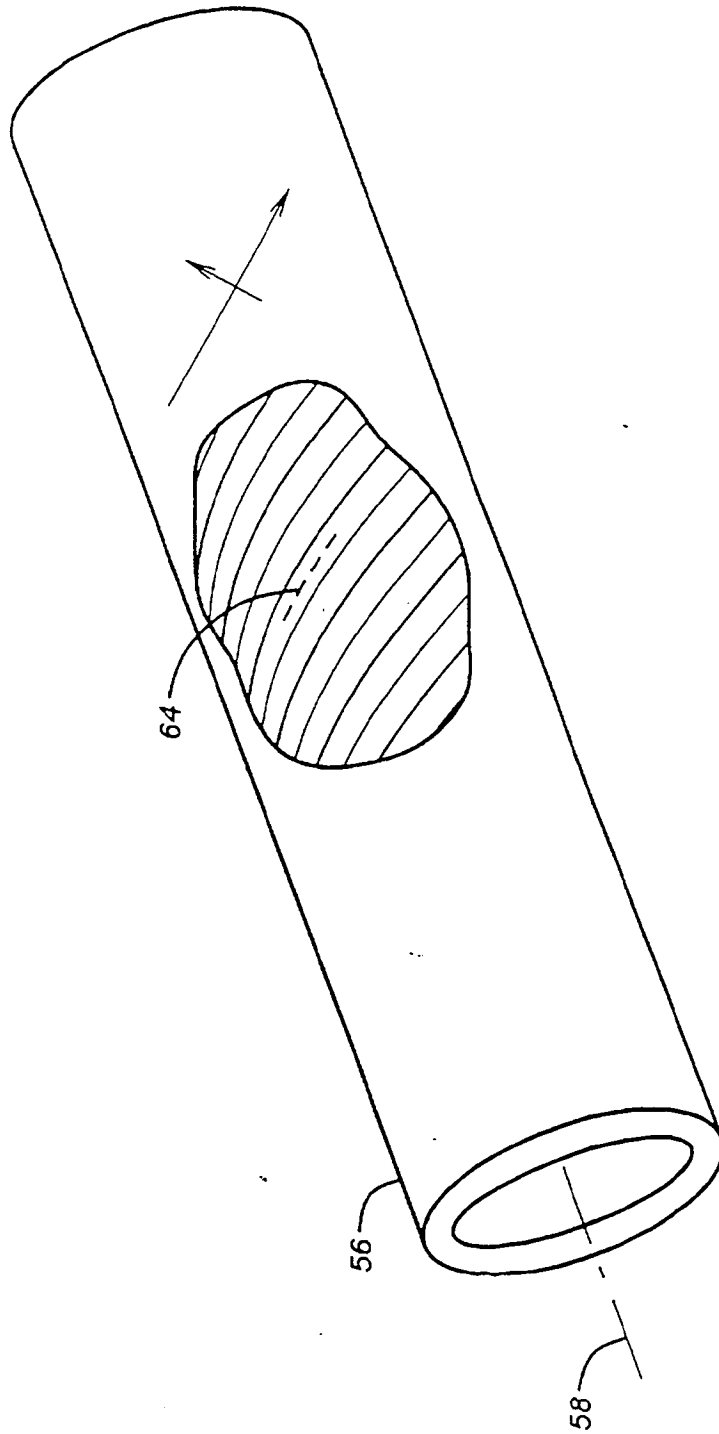
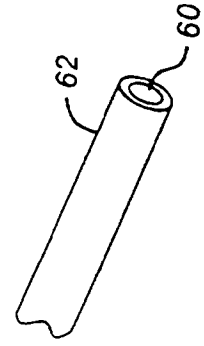


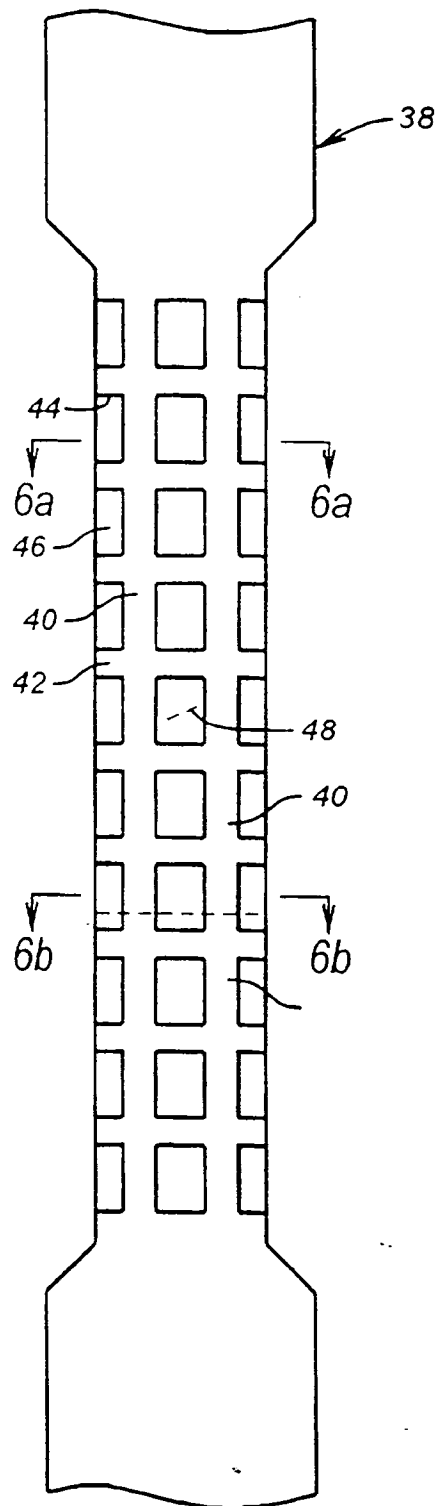
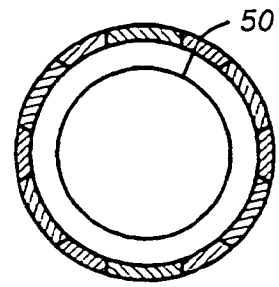
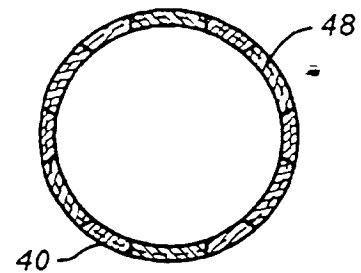
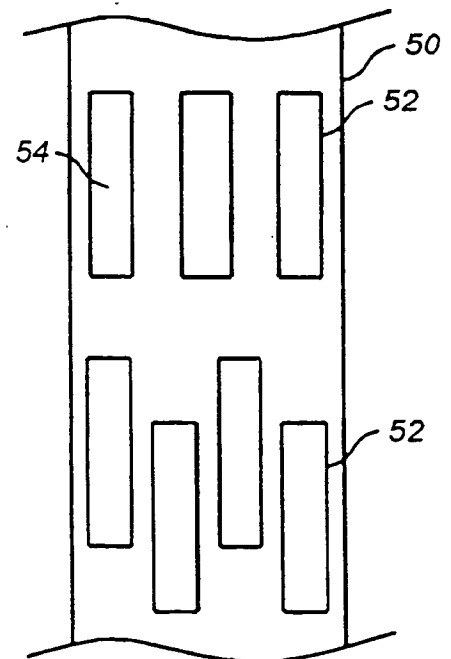
FIG. 3

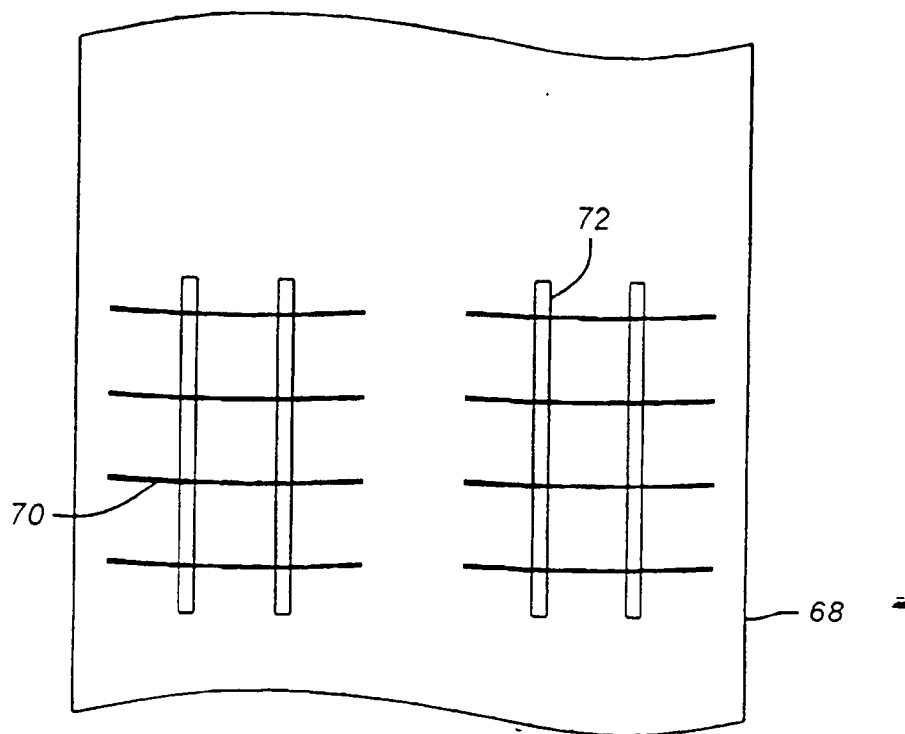
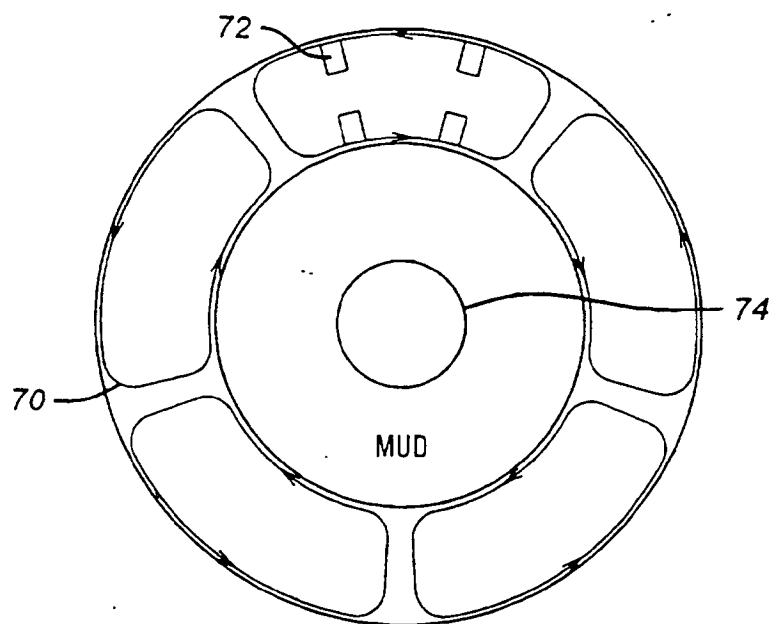


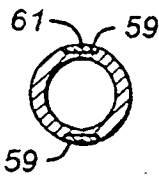
**FIG. 4**



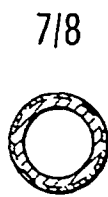
**FIG. 5**

**FIG. 6****FIG. 6a****FIG. 6b****FIG. 7**

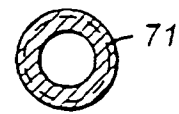
**FIG. 8****FIG. 9**



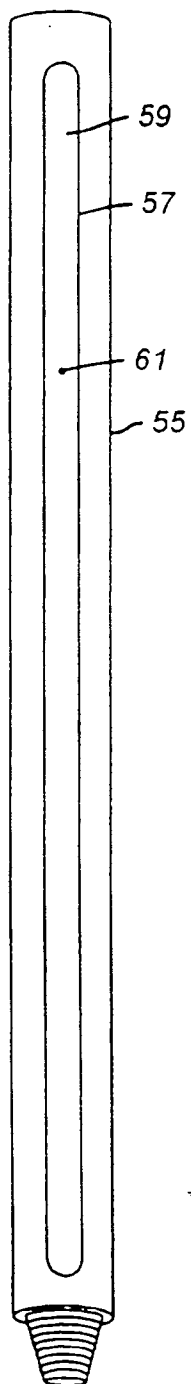
**FIG. 11**



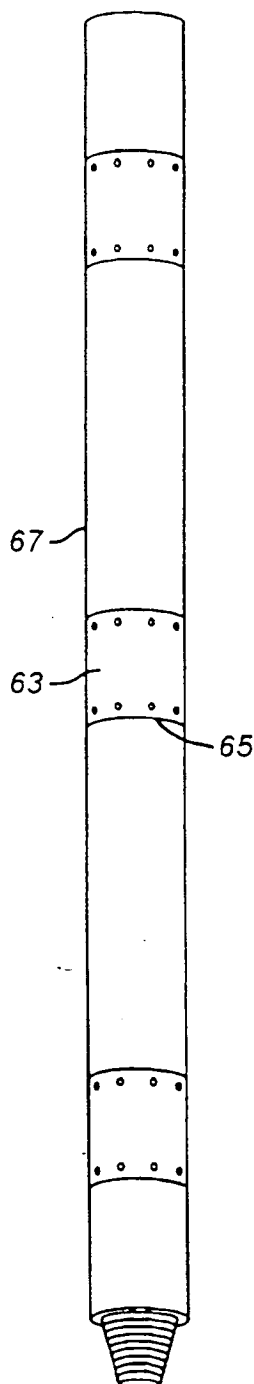
**FIG. 13**



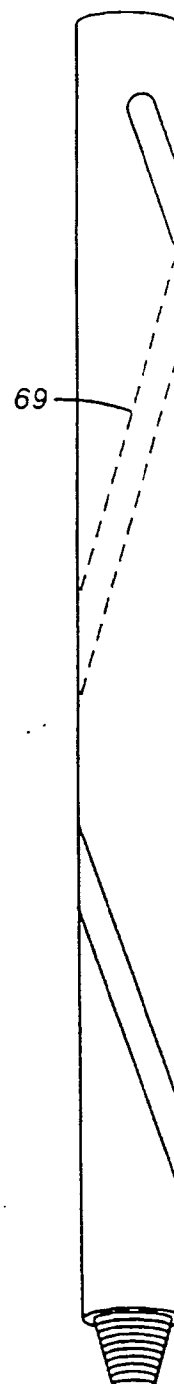
**FIG. 15**



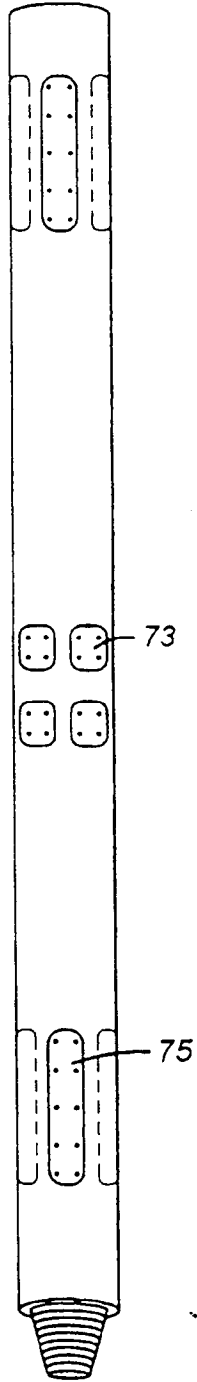
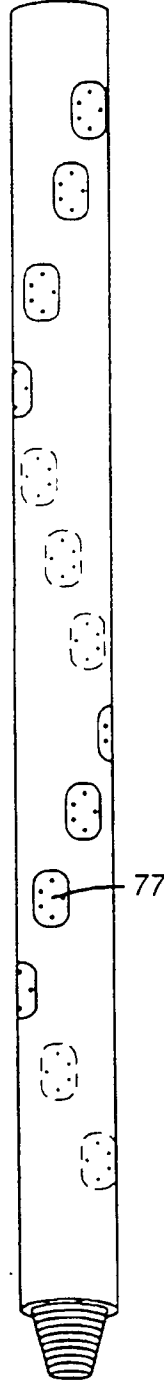
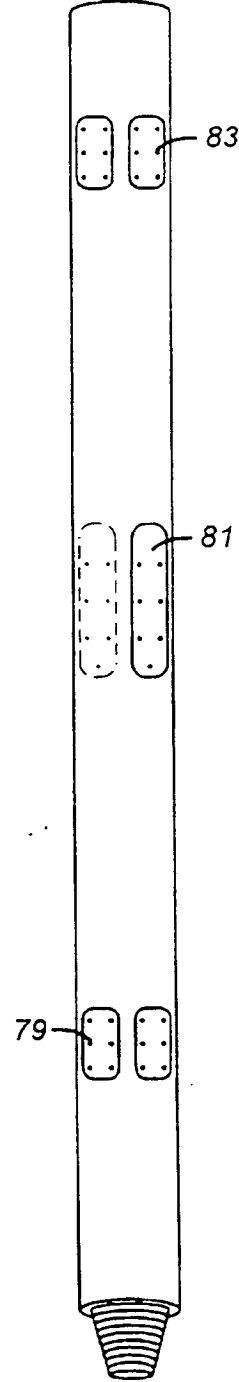
**FIG. 10**



**FIG. 12**



**FIG. 14**

**FIG. 16****FIG. 17****FIG. 18**

**DRILLPIPE STRUCTURES TO ACCOMMODATE  
DOWNHOLE TESTING**

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15 The field of this invention relates to drillpipe structures which can accommodate the loads imposed during drilling, while at the same time facilitate making a variety of measurements while drilling.

20 Present drilling technology incorporates a metal tubular connecting the surface drilling equipment to the drill bit at the bottom of the well. One of the difficulties in the design of measurement-while-drilling (MWD) tools is that they need to be attached to the drill string without undue encumbrances of the drilling operation. The bottom of the drill string where the MWD tools are located is usually composed of metal tubulars called collars, which have to  
25 provide mechanical integrity and sometimes weight to the drill string while conveying drilling fluid from the surface to the bit. MWD sensors are either mounted on and integral to the collar or are housed in a central package inside the bores of the collars. Certain formation sensor transducers, such as

formation resistivity sensor antennas, are restricted from being located inside the collar bores because the metal walls seriously degrade their ability to measure wellbore parameters outside the collars. This inability to "see through" the collar walls usually causes certain MWD tools to be more expensive to build and maintain than central "sonde"-based tools.

Antennas which are housed or attached to the various components of the drill string are used in MWD applications either to enable measurements of electrical parameters in the downhole environment or to enable communication of information with the surface or other drill string components. A challenge in making an antenna go downhole in a drilling environment requires satisfaction of both electrical and mechanical constraints. One particular type of antenna is the transverse electric type in which current flows around the drill string component in which the antenna is contained. The drill string component is usually a drill collar and the result of the current flow is to induce, in the case of a transmitting antenna, a magnetic field in the region around the antenna. In the situation of a receiving antenna, the magnetic field, which is locally axial in a direction along the drill string, induces current in the antenna element or elements which are around the drill string component in an azimuthal direction. Transmitting and receiving antennas are similar in construction, the difference being the direction of energy flow. A gap has to be maintained between the azimuthal current element and the high-conducting drill string in order for the magnetic field to encircle the element and thereby allow energy flow to or from the downhole environment proximate to the antenna.

One technique in the construction of antennas has been to neck down the highly electrically conducting drill collar in the antenna region, so that the antenna element does not extend out past the radius of the collar in order to protect it from the drilling environment. The region around the antenna element is then covered with electrical non- or semiconducting materials such as fiberglass, ceramic and rubber, to protect the element from the drilling environment. Another design is to neck down the drill collar but to use a slotted mask in place around the antenna element. The mask provides more protection from the drilling environment than other methods and the mask also provides electrical shielding necessary in these applications. The axial slots are cut in the mask to allow the magnetic fields to pass from the region inside the metal mask, where the antenna element is contained, to the region outside so that the fields may be either received or caused in the region adjacent the drill string.

These methods involve the weakening of the drill string due to the neck down region which has been described for placement of the antenna. The presence of material in the outer diameter of the drill string is important in determining its strength, which is critical in the smaller drill collar sizes.

Composite drill type has been used as described in U.S. Patent 5,332,049. This type of hybrid structure of a composite with hardened steel end fittings suffers drawbacks of failures at the juncture of the metallic and composite segments. Additionally, such designs of composites have included fibers applied in layers successively over each other, where each layer was made entirely of one kind of fiber, such as carbon or glass fiber. Successive layers were placed one over the other during construction, until the tube was

complete. The layers which were made entirely of carbon fibers had the disadvantage that they prevented the passage of electromagnetic energy. Other constructions which involved composites used to provide strength to resist internal pressures are known but are unsuitable for drilling application.

5 Some examples of such construction for cables or tubular goods employing layers of composite materials include U.S. Patents Nos. 5,110,644, 5,234,058 and 5,172,765.

Even the composite materials which have been introduced for drilling applications are made of a hybrid glass/carbon fiber-reinforced epoxy and are

10 not conducive to permit electromagnetic energy to exit and reenter in the azimuthal direction for facilitating MWD of such formation features as resistivity.

Accordingly, what is desired and is an objective of the present invention is to provide a drill collar structure that has sufficient structural rigidity to

15 withstand the rigors of drilling. At the same time, the structure should be capable of supporting the MWD equipment, some types of which rely on electromagnetic energy for the measurements taken during drilling activity. Thus, the composite structure of the present invention has the objective of allowing electromagnetic energy to exit and reenter, as well as to facilitate the

20 location and operation of other borehole property measuring equipment, so that the entire assembly functions to allow real-time data of borehole conditions while at the same time facilitating the drilling operation. These objectives have been addressed in a plurality of alternative embodiments which are designed to address the two main criteria of sufficient physical rigidity of the

drill collar assembly, while at the same time the facilitation of the measurements needed during the drilling operation.

5           A drill collar structure to facilitate measurement-while-drilling (MWD) techniques while at the same time having sufficient rigidity to facilitate the drilling operation is disclosed. In some embodiments, a metal structure involving openings such as slots, preferably oriented longitudinally along its axis, but also in other configurations, are disclosed to allow sufficient strength  
10 while at the same time allowing exit and entrance of electromagnetic energy. A composite structure is also disclosed which, for given layers, has adjacent fibers such as glass and carbon, so that when the layers are overlapped, glass areas overlap glass areas throughout the radial thickness of the composite tube to create "windows" for the entrance and exit of electromagnetic  
15 energy. In yet other embodiments, the drill collar can be made of a metallic frame structure with a multiplicity of openings which are filled with a composite material. The metallic frame structure provides structural rigidity while the openings, filled with composite material which are attached to the metal structure, form a fluid-tight cohesive structure sufficient to withstand the rigors  
20 of drilling, while at the same time allow the measurements of the formation to be taken through the windows or by making use of sensors embedded in the windows. In another alternative composite structure, carbon fibers can be used if they are electrically insulated in the areas where electromagnetic energy is to enter and exit the structure. Another composite alternative is to  
25 alternate carbon and glass fibers in particular sequences or to use insulated

carbon fibers to facilitate the operation of instruments which can be mounted in the structure whose operation could be negatively affected by conductivity in the wall in an azimuthal direction.

5 Various embodiments of the present invention will now be described, by way of example only, and with reference to the accompanying drawings in which:

Figure 1 is a perspective view of a layer making up a piece of a composite tubular drill collar for support of MWD equipment to permit electromagnetic waves to exit and enter.

10 Figure 2 is a view of Figure 1, showing overlapping layers of glass fibers creating diamond-shaped windows in the composite structure.

Figure 3 is a further development of Figure 2, also in perspective, illustrating how the overlapping glass fibers create windows in the composite drill collar.

15 Figure 4 is an alternative embodiment of a composite drill collar which facilitates MWD by virtue of the fiber orientation of the layers.

Figure 5 is a detail of one of the fibers usable in the application of Figure 4.

20 Figure 6 is an alternative embodiment showing in sectional elevational view a drill collar with a metallic framework defining a plurality of windows which can be filled with composite materials.

Figure 7 is a sectional elevational view of a metallic drill collar showing alternative layouts of openings, which can be of a variety of shapes, and in the upper segments shown to be aligned, while in the lower segment are shown to be offset but overlapping.

Figure 8 is an elevational view of a composite drill collar, showing wire loops embedded in the collar.

Figure 9 is a section view through Figure 8, showing how a sonde-mounted antenna creates a magnetic field which induces current in the wire loops embedded in the composite so as to create a field in the surrounding formation.

Figure 10 is an elevational view of an elongated window found in a groove on a section of a drill collar, showing an orientation of two windows at 180°.

Figure 11 is a section view through Figure 10, showing the location of the windows.

Figure 12 is an alternative to Figure 10, showing three spaced-apart bands forming the windows.

Figure 13 is a section through one of the windows of Figure 12.

Figure 14 is yet another alternative, showing a spiral window.

Figure 15 is a section through Figure 14.

Figures 16, 17, and 18 are further alternative embodiments of window layouts on a metallic drill collar where an opening goes through the wall and is covered.

One way to address the fabrication of a drill collar 10 with a composite structure, which facilitates the passage of electromagnetic energy through it, is shown in Figures 1-3. A single layer is illustrated in Figure 1, which has a band 12 of glass fibers, in the preferred embodiment sandwiched between

bands 14 and 16 of preferably carbon fibers. Those skilled in the art will appreciate that band 12 can be formed from any material that is not a barrier to electromagnetic energy in a helical direction as represented by arrow 18 of Figure 3. Figure 2 illustrates the overlay of layers wherein each of the layers 20 and 22 are formed with the alternating pattern depicted in Figure 1, for example, glass fibers 12 between carbon fibers 14 and 16. The overlay of bands 20 and 22, which are helically wound to create the collar 10 at angles which can vary in a particular design, is to create an overlapping area, shown more specifically by points 24 through 30. Where measured in a radial direction, *i.e.*, at 90° to longitudinal axis 32 and between points 24, 26, 28, and 30, there exist only glass fibers 12, as indicated schematically in Figure 3 for two adjacent layers. Thus, regardless of the degree of the helix formed by each band, which is itself a function of the ultimate desired structural strength, and regardless of how many bands overlap each other to form the composite which makes up the drill collar 10, the objective is to create a collar 10 to have sufficient structural rigidity to withstand the rigors of drilling and the pressures internally from the circulating mud, while at the same time to create overlapping strips of material which can pass electromagnetic energy as identified by points 24, 26, 28, and 30, also known as "windows." Those skilled in the art will appreciate that depending on the diameter of the drill collar 10 to be produced and the angle used for the helical winding of the individual layers such as 20 and 22, two or more windows in a given elevation will be created. The spacing of the rows of windows is also dependent on the helical angle of the wrap of the bands 20 and 22. However, regardless of how many bands it takes to get the resulting structural rigidity and the ability to withstand inter-

nal pressures, the construction techniques illustrated result in the creation of windows at periodic intervals where desired along the length of the collar **10**. These windows are at a given elevation along the collar **10** and can pass electromagnetic energy.

5           Shown schematically as **32** in Figure 3, the transmitting or receiving antennas can be embedded within the wall **34** of drill collar **10**. Alternatively,

the transmitting and receiving antennas can be mounted on a separate sonde and placed into position in the drill string within the composite drill collar **10** depicted in Figures 1–3. Flow can go around or through the sonde, which is  
10 not shown in Figure 3 but is schematically depicted in Figure 6A or an alternative embodiment. This application will be described below. However, it is within the scope of the invention to mount the transmitters and receivers or other instrumentation generally within the wall **34** of the drill collar **10** or within  
15 the internal bore **36** so that the instrumentation can be separately handled and installed in the collar **10** after the drill string is made up.

Figure 6 illustrates an alternative embodiment involving a collar **38**, which is generally of a metallic structure comprising a framework of longitudinal members **40** and transverse members **42**, which collectively describe a  
20 plurality of openings or windows **44**. The number of openings is exaggerated to illustrate a particular layout. Fewer openings can be employed. Each of the windows is sealed off with a cover **46** that, in the preferred embodiment, is made from a composite material such that the tubular **38** can conduct drilling fluids to the drill bit. The array of the metallic structure can be varied. The combination of the

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covers 46 with the longitudinal and transverse members 40 and 42 acts as a unified structure because not only do the covers 46 seal off the openings 44, they interact with the framework of the tubular 38 through the longitudinal and transverse members 40 and 42 to create a unified structure to resist the applied stresses during the drilling operation. The windows 44 can, if made of the right materials, allow for the passage of electromagnetic waves to facilitate the resistivity measurements while drilling. The number and placement of the windows 44 can be adjusted to accommodate the particular MWD instrumentation to be mounted in the collar 38, as well as at the same time to provide sufficient strength for the overall assembly of the collar 38 to withstand the rigors of drilling. The covers 46 can be made of any composite material sufficiently strong to add to the structural strength of the framework of longitudinal and transverse members 40 and 42 and, in certain applications, allow electromagnetic waves to exit and enter to facilitate certain measurements. It can include fiber reinforcement comprising long fibers, short fibers, or particles. The matrix can utilize all types of thermosetting polymers with increased temperature and fluid resistance, thermoplastic polymers with high temperature fluid resistance, ceramics, and also metallic materials if special properties are required. The fibers can be particles of glass, ceramic, and polymers if electromagnetic transparency and electric resistance are required. Carbon fibers, steel fibers, or other conductive materials can be used where no requirements regarding electromagnetic transparency or electric resistance are required. Different combinations of fibers and matrices can be used for the cover 46 to obtain different mechanical and physical properties for a particular application.

Sensors 48, shown schematically in Figure 6, can be embedded in the covers 46. Alternatively, as shown in Figure 6A, a sonde 50 can be inserted into the tubular 38 such that the sensors 48, or antennas or the like, are positioned adjacent to the covers 46 within the tubular 38. Alternatively, as shown in Figure 6B, the sensors, transmitters or receivers shown schematically as 48 can be mounted within the covers 46 and can actually circumscribe the tubular 38 as the sensors are strung through longitudinal members 40 and into adjacent covers 46, as shown in Figure 6B. Appropriate installation can be provided around the antenna or other sensor 48 as it goes through the longitudinal member 40.

The type of instrumentation that is used with collar 38 can include electromagnetic, gamma ray density, NMR, acoustic, resistivity, directional, pressure, fiber optic, optical distance chemical analysis (spectroscopy), borehole scope, stress measurement in collar 38 including windows 46, vibration, and other applied mechanical forces.

The arrangement of the openings 44 can vary from that as shown in Figure 6. The structure overall must have the requisite rigidity to withstand the rigors of drilling, and the placement of the openings 44 needs to take the structural requirements into account while providing windows at the appropriate location to facilitate the MWD measurements. The sensors 48 can provide information about the surrounding environment outside the collar 38 or about conditions within the collar 38 as well as conditions within the wall of the collar 38, such as the stresses acting on the covers 46 or the structural members 40 and 42. The collar 38 would have the traditional metallic threaded ends so it could be

included into a drill string. The covers 46 can be joined to the framework of members 40 and 42 by use of screws, bolts, clamps, or the like. The shape of the openings 44 can also vary. Accordingly, a tubular such as 38 can have a series of round holes drilled into it to act as the openings 44 which are filled with composite covers 46.

The structure shown in Figure 6 and its equivalents can be substantially stronger than a tubular made entirely of composite materials in combination with steel tool joints. Such structures, such as shown in U.S. patent 5,332,049, in the past have shown weakness and a tendency of stress failure at the transition of the steel tool joint to the composite tube wall body. The type of structure such as illustrated in Figure 6 by virtue of a metallic base structure can minimize this problem.

Figure 7 is an alternative embodiment illustrating a metallic tubular structure 50 for the collar with a series of longitudinal openings 52. Openings 52 may be in alignment, as shown in the top of Figure 7, or may be offset, as shown near the bottom of Figure 7. Other patterns for the openings can also be used. The presence of the openings eliminates or reduces conductivity in the azimuthal direction and allows various sensors to be mounted within covers 54, which are in openings 52, or sensors mounted on a sonde (not shown) which can be easily inserted into the drill string from the surface for proper positioning of such elements as antennas in the vicinity of the openings 52. Electromagnetic energy can pass through these openings. The structure in Figure 7 can also have a composite structure by using carbon and/or glass fibers, for example, in combination with openings such as 52 to further pro-

mote the ability to facilitate the workings of instruments employing magnetic dipoles in longitudinal directions or coils oriented in a longitudinal orientation.

Figures 10–18 illustrate other alternative embodiments using a tubular structure 55 for the drill collar, wherein windows such as 57, shown in Figure 10, are accomplished using an outer wall recess into which is disposed a composite material 59. Thus, the strength of using a metallic material or other high-strength material for the tubular 55 is obtained while at the same time, sensors, schematically shown as 61, can be embedded in the composite windows 59. While Figure 10 illustrates a pair of opposed longitudinal recesses in which the composite windows 59 are mounted, different shapes can also be used. Thus, Figure 12 shows a series of windows 63 which extend in recesses 65 which extend around the periphery of the tubular 67, which preferably of a rigid or metallic structure. Figure 14 is a variation showing a spiral groove 69 into which the composite window material 71 is mounted. Figures 16–18 show similar structures involving recesses or openings through the entire wall, with composite windows in the recesses in a variety of orientations and shapes. In Figure 16, the middle of the tubular has two rows of four square windows 73, and above and below are individual rows of three oblong windows 75 at 120° from each other. Figure 17 uses square windows 77 in the spiral pattern, while Figure 18 shows a bottom row of four oblong windows 79 disposed at 90°, a middle row of oblong windows 81 equally spaced at 180° or 120°, and an upper row of oblong windows 83 at 90° from each other. In the various embodiments of Figures 10–15, the underlying drill collar does not have the entirety of its wall removed to create a window. Instead, a recess in its outer

surface is provided in any given shapes and arrays on its outer periphery so that the composite material can be inserted therein with the sensors in the composite material or directly beneath it. Some communication opening through the wall or alternatively, exteriorly outside the wall of the tubular, is provided to allow connection of the sensors, such as 61 in Figure 11, so that the readings obtained can be processed by the downhole equipment, as well as to provide the necessary power supply such as, for example, where a transmitter is located. Power and signals can thus be wired in the wall or wireless communication over a short distance can be used as with a sonde, for example. A sonde can be used to connect signal and power wires to a sensor in the window. A sensor can be on the sonde and extendable to the window through access through an opening in the tubular wall. Accordingly, as used in this specification, "openings" is intended to encompass voids through the wall of the tubular as well as recesses in its outer surface to accommodate a window which is preferably of a composite material.

Referring now to Figure 4, another tubular structure for a collar 56 is shown. In the cutaway view, a series of fibers is shown substantially transverse to the longitudinal axis 58. In the cutaway segments, a series of parallel lines represent adjacent fibers which can be oriented in certain predetermined sequences. For example, the fibers can alternate between carbon fiber and glass fiber, where every other fiber is carbon, sandwiched in between a pair of glass fibers. Alternatively, several carbon fibers can be adjacent to each other separated by a glass fiber and the pattern repeating itself. Alternatively, as shown in Figure 5, carbon fibers 60 can be used which are covered with electrical insulation 62. When so insulated, the carbon fibers, which if helically

wrapped would have a vector component in the azimuthal direction, are rendered less conductive in the azimuthal direction due to the insulation.

While the fibers in Figure 4 are shown nearly transverse (at 90°) to the longitudinal axis 58, other orientations for the fibers of each of the layers can

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be employed. The significance of the embodiment illustrated in Figure 4 is that conductivity in the azimuthal direction is reduced, which enhances the effectiveness of the some of the instrumentation for MWD, which can be supported on a sonde internally to the collar 56 or having portions thereof embedded in the wall. The pres-

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ence of the carbon fibers adds structural strength while the glass fibers constitute blocks to azimuthal conductivity because they form a nonconducting azimuthal gap. Thus, if the carbon fibers are used and coated as shown in Figure 5, the azimuthal component of any conduction through the carbon fibers is minimized due to the insulative effects of the insulating layer 62. The interspersing of glass fibers between carbon fibers accomplishes the same objective. Conductivity, if the fibers are spirally wound, occurs along the length of the fibers and it has a longitudinal and an azimuthal component. However, the azimuthal component encounters resistance of either the insulation 62 or, in the alternative embodiments, the interspersed glass fibers.

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Between the built-up layers which comprise the tubular 56, the antennas 64 which allow for transmission and reception of electromagnetic waves in one embodiment can be placed between or within layers adjacent nonconducting fiber components or poor conducting fiber components in the azimuthal direction. Accordingly, the structure of Figure 4 is intended to illustrate the use of a composite structure for a tubular 56 wherein the selec-

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tion and orientation of the fibers is such that conductivity azimuthally is minimized while the structural strength to withstand the rigors of drilling is optimized. By proper orientation and selection of the component fibers within the wall structure of the tubular 56, antennas for resistivity measurement or other test equipment such as nuclear magnetic resonance (NMR) can be employed with minimal interference of the transmitted or received signals due to the construction of the tubular 56, which supports the test equipment. The concept of windows can also be incorporated into the structure of Figure 4 so that electromagnetic energy can exit and enter.

Figure 8 shows an elevational view of a composite drill collar 68, showing a plurality of wire loops 70 embedded in the wall of the collar 68. Short ferrite strips 72 can be used to enhance the performance of the loops 70. As shown in Figure 9, a sonde-mounted antenna wire 74 is presented within the collar 68 in the area of loops 70. The antenna 74 induces a magnetic field which creates a current in the loops 70 which are embedded in the wall of the composite drill collar 68. The current flowing through the loops 70, in turn, induces a magnetic field in the formation surrounding the drill collar 68. Similar structures located above and/or below on the collar 68 and the sonde supporting the transmitting antenna wire 74 are used as receivers so that the desired formation properties can be measured using this technique. The composite nature of the collar 68, as previously described for the embodiments of Figures 1-4, facilitates the operation of the transmitter/receiver system illustrated in Figures 7 and 9. By virtue of selection of appropriate materials for the composite wall structure of the collar 68, the interference with the transmitted or received magnetic fields which are induced is minimized.

The foregoing disclosure and description of the invention are illustrative and explanatory thereof, and various changes in the size, shape and materials, as well as in the details of the illustrated construction, may be made.

### Claims

- 1           1.     A drill pipe, comprising:  
2                 a nonmetallic wall structure defining a flowpath and capable of  
3     withstanding the demands of drilling and comprising, at least in part, at least  
4     one component made of a material which is presented within said structure  
5     in a manner as to permit the passage of electromagnetic energy.
  
- 1           2.     The drill pipe of claim 1, wherein:  
2                 said wall structure is made in part of a composite material.
  
- 1           3.     The drill pipe of claim 2, wherein:  
2                 said wall structure comprises a plurality of layers wherein each  
3     layer is made in part of material that permits the passage of electromagnetic  
4     energy.
  
- 1           4.     The drill pipe of claim 3, wherein:  
2                 each overlapping layer is oriented with respect to its adjacent  
3     layer so that components made from a material which permits passage of  
4     electromagnetic energy overlap, at least in part, in every layer in said wall.
  
- 1           5.     The drill pipe of claim 4, wherein:  
2                 each layer comprises a plurality of carbon fibers adjacent a  
3     plurality of glass fibers.

1           6.     The drill pipe of claim 5, wherein:  
2                 said carbon and glass fibers are in alternating bands so that glass  
3     fibers in one layer overlap glass fibers in an adjacent layer, such that at least  
4     one window of overlapping glass fibers extends through said wall.

1           7.     The drill pipe of claim 1, wherein:  
2                 said wall further comprises instrumentation, located adjacent said  
3     component which permits passage of electromagnetic energy, said instru-  
4     mentation uses electromagnetic energy to measure formation properties when  
5     the drill pipe is located downhole.

1           8.     The drill pipe of claim 1, further comprising:  
2                 a sonde insertable into said flowpath to position instrumentation  
3     adjacent said component which permits passage of electromagnetic energy  
4     to facilitate use of said instrumentation in testing of a formation using electro-  
5     magnetic energy when the drill pipe is located downhole.

1           9.     The drill pipe of claim 6, wherein:  
2                 said wall further comprises instrumentation located adjacent said  
3     window which uses electromagnetic energy to measure formation properties  
4     when the drill pipe is located downhole.

1           10.    The drill pipe of claim 6, further comprising:  
2                   a sonde insertable into said flowpath to position instrumentation  
3 adjacent said window to facilitate testing of a formation using electromagnetic  
4 energy when the drill pipe is located downhole.

1           11.    A composite drill pipe to resist conductivity in an azimuthal or  
2 helical direction, comprising:  
3                   a composite tubular wall structure defining a flowpath therein and  
4 comprising at least in part fibers which, in their position in the wall structure,  
5 are not azimuthally conductive or are less azimuthally conductive than other  
6 fibers within said wall structure.

1           12.    The drill pipe of claim 11, wherein:  
2                   said wall comprises of a plurality of overlapping layers and at  
3 least one of said layers comprises an alternating pattern of more-conductive  
4 and less-conductive fibers.

1           13.    The drill pipe of claim 12, wherein:  
2                   carbon fibers are alternated with glass fibers.

1           14.    The drill pipe of claim 13, wherein:  
2                   each carbon fiber is between a glass fiber on either side.

1           15.   The drill pipe of claim 13, wherein:  
2                   a plurality of carbon fibers is between at least one glass fiber on  
3 either side.

1           16.   The drill pipe of claim 11, wherein:  
2                   at least some fibers are insulated to make them less azimuthally  
3 conductive than they would be if they were not insulated.

1           17.   The drill pipe of claim 16, wherein:  
2                   said insulated fibers comprise carbon fibers.

1           18.   The drill pipe of claim 16, wherein:  
2                   some fibers are noninsulated carbon fibers and others are insu-  
3 lated carbon fibers to form azimuthal conductivity gaps.

1           19.   The drill pipe of claim 11, further comprising:  
2                   instrumentation mounted, at least in part, in said wall for measur-  
3 ing while drilling with drill pipe where reduced azimuthal conductivity facilitates  
4 the measurement.

1           20.   The drill pipe of claim 11, further comprising:  
2                   instrumentation mounted to a sonde insertable into said flowpath  
3 for measuring while drilling with drill pipe where reduced azimuthal conductiv-  
4 ity facilitates the measurement.

1           21. The drill pipe of claim 13, wherein:  
2                 glass fibers overlap in every layer to create windows which allow  
3           passage of electromagnetic energy.

1           22. A drill pipe, comprising:  
2                 a tubular metallic structure defining a plurality of voids or re-  
3           cesses on an outer surface referred to as openings;  
4                 covers in said openings attached to said tubular structure to allow  
5           the assembly to withstand applied stresses during drilling while facilitating  
6           measurement while drilling through said openings.

1           23. The drill pipe of claim 22, further comprising:  
2                 instrumentation mounted at least in part in said covers to facilitate  
3           at least one of (1) downhole measurements of the surrounding formation  
4           outside said tubular structure, (2) measurements of fluid conditions within the  
5           tubular structure, or (3) measurement of the conditions of the covers.

1           24. The drill pipe of claim 22, further comprising:  
2                 instrumentation mounted on a sonde and supported within the  
3           tubular structure so that measurements of fluid conditions within said tubular  
4           structure or of formation properties outside said tubular structure through said  
5           covers can be accomplished.

1           25. The drill pipe of claim 22, wherein:  
2                 said covers allow passage of electromagnetic energy.

1           26.    The drill pipe of claim 25, wherein:  
2                   said covers are secured to said metallic structure in a load-  
3 bearing manner so as to withstand applied stresses which occur during  
4 drilling.

1           27.    The drill pipe of claim 25, wherein:  
2                   said covers are made of a composite material.

1           28.    The drill pipe of claim 27, wherein:  
2                   said covers comprise fiber reinforcement.

1           29.    The drill pipe of claim 28, wherein:  
2                   said openings are elongated and aligned with a longitudinal axis  
3 of said metallic structure.

1           30.    The drill pipe of claim 28, wherein:  
2                   said openings are randomly disposed in said structure.

1           31.    The drill pipe of claim 22, wherein:  
2                   said structure further comprises metallic thread at each end for  
3 connection down to a drill string.

1           32.    The drill pipe of claim 23, wherein:  
2                   said instrumentation performs at least one of the following mea-  
3 surements: electromagnetic, gamma ray density, NMR, acoustic, resistivity,

4 directional, pressure, fiber optic, optical distance chemical analysis (spectro-  
5 scopy), borehole scope, stress measurement in said metallic structure or said  
6 covers, vibration, and other applied mechanical forces.

1 33. The drill pipe of claim 24, wherein:

2 said instrumentation performs at least one of the following mea-  
3 surements: electromagnetic, gamma ray density, NMR, acoustic, resistivity,  
4 directional, pressure, fiber optic, optical distance chemical analysis (spectro-  
5 scopy), borehole scope, stress measurement in said metallic structure or said  
6 covers, vibration, and other applied mechanical forces.

1 34. The drill pipe of claim 24, wherein:

2 said instrumentation on said sonde comprises at least one an-  
3 tenna;

4 said wall comprises at least one electrically conductive loop;

5 wherein said antenna creates current through said loop by gen-  
6 erating a magnetic field, which in turn allows said loop to create a magnetic  
7 field into the surrounding formation through said wall.

1 35. The drill pipe of claim 34, wherein:

2 said sonde comprises a transmitting antenna to broadcast a  
3 magnetic field into the formation using a plurality of said loops and where  
4 another antenna receives the magnetic field which returns from the formation.

36. The drill pipe of claim 28, wherein said openings are spirally wound on said structure.

37. A tubular drill collar comprising at least one composite layer, said composite layer comprising a band of substantially non-conductive fibers disposed between adjacent bands of substantially conductive fibers, said band of non-conductive fibers permitting, in use, the passage of electromagnetic energy.

38. A tubular drill collar as claimed in claim 37, wherein said bands comprise one or more fibers.

39. A tubular drill collar as claimed in claim 37 or 38, wherein said non-conductive fibers are glass, ceramic or polymer fibers, or normally conductive fibers covered with an electrically insulating material.

40. A tubular drill collar as claimed in any of claims 37, 38 or 39, wherein said conductive fibers are carbon or steel fibers.

41. Measurement-whilst-drilling apparatus comprising a tubular drill collar as claimed in any of claims 37-40.

42. Measurement-whilst-drilling apparatus as claimed in claim 41, further comprising measurement means for measuring the resistivity of a formation surrounding a wellbore, said measurement means being arranged to transmit and receive electromagnetic energy via said band of non-conductive fibers.

43. A method of making a tubular drill collar comprising the step of:

providing at least one composite layer, said composite layer comprising a band of substantially non-conductive fibers disposed between adjacent bands of substantially conductive fibers, said band of non-

conductive fibers permitting, in use, the passage of electromagnetic energy.

44. A tubular drill collar substantially as  
5 hereinbefore described with reference to the  
accompanying drawings.



Application No: GB 9911561.0  
Claims searched: 1 - 21

Examiner: Andrew P Jenner  
Date of search: 14 July 1999

**Patents Act 1977**  
**Search Report under Section 17**

**Databases searched:**

UK Patent Office collections, including GB, EP, WO & US patent specifications, in:

UK Cl (Ed.Q): E1F: FAC, FHK, FHU

Int Cl (Ed.6): E21B: 17/00, 17/20, 47/12

Other: EPODOC, World Patents Index, JAPIO

**Documents considered to be relevant:**

Category	Identity of document and relevant passage	Relevant to claims
X	EP 0816632 A1 GEOSERVICES - whole document relevant	1 - 7, 9, 37 - 40, 43
X	EP 0274457 A2 HUGHES et al - whole document relevant	1, 7 - 10, 37, 41 - 43
X	WO97/21117 A1 POMERLEAU - whole document relevant	1 - 7, 9, 11 - 15, 37 - 41, 43

X	Document indicating lack of novelty or inventive step	A	Document indicating technological background and/or state of the art.
Y	Document indicating lack of inventive step if combined with one or more other documents of same category.	P	Document published on or after the declared priority date but before the filing date of this invention.
&	Member of the same patent family	E	Patent document published on or after, but with priority date earlier than, the filing date of this application.